© Copyright Statement

All rights reserved. All material in this document is, unless otherwise stated, the property of **FPC International, Inc**. Copyright and other intellectual property laws protect these materials. Reproduction or retransmission of the materials, in whole or in part, in any manner, without the prior written consent of the copyright holder, is a violation of copyright law.

Evaluation of FTC-1 Combustion Catalyst at BHP#Utah Coal Ltd's Peak Downs mine by:

(i) AS2077-1982 Method for Fuel Cons. (ii) ASTM D2156-63T for Black Smoke (iii) Examination of Daily Fuel Usage

March, 1991

Submitted by: Brid Walker

Fuel Technology Pty Ltd 58 Antimony St CAROLE PARK 4300 Ph (07) 271 4138 Fax (07) 271 3737

TABLE OF CONTENTS

INTRODUCTION

AS 2077-1982 METHOD OF FUEL CONSUMPTION MEASUREMENT
ASTH D2156-63T METHOD, Bacharach Smoke Patch Test
EXAMINATION OF DAILY FLEET FUEL USAGE
CONCLUSIONS
APPENDIX I AS 2077-1982 DESCRIPTION
APPENDIX II: AS 2077-1982 RESULTS
APPENDIX III: ASTM D2156-63T, Bacharach Smoke Patches
APPENDIX IV: DAILY FUEL CONSUMPTION GRAPH

÷

INTRODUCTION:

FTC-1 is a combustion catalyst which, when added to liquid petroleum fuels, accelerates the chemistry of combustion, allowing the fuel to burn faster and more thoroughly. Typical fuel savings of 6-8% are generated for mobile equipment.

Because of the many variables that affect fuel consumption in the mining environment, it can be very difficult to accurately quantify these benefits using field records. For this reason, Fuel Technology Pty Ltd use the AS 2077-1982 method, which measures the amount of "burnt fuel leaving the engine" under repeatable static test conditions.

1. AS 2077-1982 METHOD OF FUEL CONSUMPTION MEASUREMENT

This method measures the amount of carbon leaving the engine via the exhaust, which is proportional to the amount of fuel entering the engine. A percentage change measured accurately reflects the same change in fuel consumption occurring.

The value of this method is threefold:

- Test conditions can be repeated. Any changes in climatic condition, etc is recorded so that comparisons can be made at conditions of standard temperature and pressure.
- (ii) Test accurately reflects field benefits, providing that a static load is applied to the test engines.

(iii) Easy and inexpensive to conduct.

Full details of procedures appear in Appendix I.

Engines to be tested were at operating temperature, and set at 1800 rpm for the test. <u>No load was applied</u>! Three CH200 coal haulers

were tested prior to, and after fuel treatment. Full test data and results appear in Appendix II of this report.

Results Summary:

Table I

| Hauler No | Carbo BASELINE | n Flow Rate TREATED | % Change In Fuel Con | з, |
|--------------|-------------------|------------------------|-------------------------|----|
| 24 | 13.604 | 7.626 | -43.9 See <u>Mote</u> ! | |
| 25 | 6.019 | 5.089 | -15.4 | |
| 64 | 7.863 | 7.034 | -10.6 | |
| Average | | | -13.0% | |

<u>Note</u>: This engine was running hot during baseline test. (Exhaust temperature 386°C compared to 197°C during treated test.) It was subsequently discovered that the coolant level was low. This would have resulted in increased frictional losses and very poor baseline efficiency. The results were therefore deleted from the average.

N.B. <u>Comments</u>: These tests were performed at "fast idle" (1800 rpm no load). Combustion efficiency under these conditions is less than optimum, hence the magnitude of the catalyst's action is greater. Similar tests conducted at CRA's Tarong Coal operations showed an average 12.6% fuel saving at idle, and 7.1% under static load, the latter more closely reflecting field results.

2. ASTM D2156-63T METHOD. Bacharach Smoke Patch Test

This test involves sampling a standard volume of exhaust gas, taken under test conditions as set out in AS 2077-1982. The exhaust gas sample is passed through a filter paper and the degree of discolouration caused by the particulate matter is determined against a series of standards. Copy of exhaust patches appears in Appendix III.

Results Summary:

Table II

| Hauler No | Bacharac FASELINE | h Smoke No TREATED | % Change |
|--------------|----------------------|-----------------------|----------|
| 24 | 6.5 | 4.0 | -38.5 |
| 25 | 6.0 | 4.0 | -33.3 |
| 64 | 5.0 | 3.5 | -30.0 |
| AVERAGE | | | -34.3% |

<u>Comments</u>: The improvements in emissions of exhaust particulates also confirms a fuel efficiency improvement, but of course, this procedure provides no means of quantifying it.

3. EXAMINATION OF DAILY FLEET FUEL USAGE

The total fuel usage (in litres) by mobile equipment has been monitored on a daily basis, except for weekend usage, since 19.10.90, approx. $5^1/_2$ weeks prior to commencement of fuel treatment. At this stage, equipment operating hours have not been incorporated. By graphing the <u>daily</u> figures, there should be sufficient statistical data to detect a trend in changed usage rate, assuming of course, that there have been no significant and sustained changes in mine `operating conditions.

Any "abnormal" days, such as those caused by strikes, etc are readily detected on the graph, and only the entries in the "high density" region of the graph are useful for comparison, since these reflect typical operating days.

Typical operating conditions occurred during the untreated period (19.10.90-27.11.90) and throughout the first few weeks of fuel treatment to 20.12.90.

The graph (Appendix IV) shows an 8.5% fall in daily fuel usage

coinciding with fuel treatment. After this period, however, operating conditions changed dramatically.

With the introduction of 2 new Le Torneau 1100 loaders, the major flooding from end-Dec to January, 1991, and the increased usage of dewatering pumps, which with the new loaders, have accounted for an additional fuel usage of up to an estimated 14,500 L/day, daily fuel consumption has varied substantially.

<u>Comments</u>: With respect to the dewatering pumps, since their operating conditions would be reasonable steady, estimates of fuel usage can be made by the following formula:

Fuel used/day = SFC (L/KWhr) x Max Power (KW) x % Duty x op.hrs

Discussions with Hanson Sykes Pumps have indicated

SFC (spec fiel cons) = .35 L/KWhr

and

% Duty = 60-70%

It could be assumed that the pumps would operate 22 hrs/day. A knowledge of what pumps were operating and on what days would provide the balance of imformation required for estimations.

Likewise, Blackwood Hodge give estimates of 120-132L/hr for the Marathon Le Tornezu 1100 loaders.

CONCLUSIONS:

1. The AS 2077-1982 fuel consumption measurements demonstrated fuel savings benefits which would support a fleet benefit of 6-8%.

2. Strong reductions of 34.3% in exhaust smoke emissions further confirm a much improved engine efficiency.

3. Initial mine records have indicated an 8.5% fuel saving.

4. Daily fuel records will require adjustments for usage of pumps and new loaders to enable comparison with "original" fleet (untreated).

۰ ...

APPENDIX II

AS 2077-1982 RESULTS: Fuel Consumption Measurements

FUEL TECHNOLOGY PTY LTD

.

CARBON BALANCE RESULTS

.

| | 1 | BUCL - PEAK | DOWNS | ĻĊ | CATION : | PEAK DOWNS | | |
|--|---|---|---------------------------------|--|--|--|------------------------------------|--------------------------------------|
| EQUIPMENT | : | EUCLID CH20 | 0 | UN | HT NR. ; | 24 | | |
| ENG. TYPE | : | CUMMINS | | MC | DEL : | KTTA38C | | |
| RATING | : | 1350 HP | | FL | JEL : | | | |
| BASELINE | | | | D/ | NTE : | 15,11,90 | | |
| ENG. HOURS | t | 1837.7 | | TE | ST MODE: | 1800 rpm | | |
| AMB. TEMP (C) | : | 32 | | S | TACK(mm): | 290 | | |
| BAROMETRIC(mb) | t | 987 | | FI | JEL DENS: | | | |
| | | TEST I | TEST 2 | TEST 3 | TEST 4 | TEST 5 | AVERAGE | \$ ST.DEV |
| PRES DIFF (Pa) | : | б0 | 68 | 67 | 69 | 70 | 67 | 5.93 |
| EXHST TEMP (C) | | 378 | 382 | 387 | 389 | 392 | 386 | 1.45 |
| HC (ppm) | | | 30 | 30 | 30 | 30 | 28.0 | 15,97 |
| CO (\$) | ; | | 0.02 | 0.02 | 0.02 | 0.01 | 0.016 | 24 23 |
| | 1 | | 7.29 | 7.29 | 7.24 | 7.28 | 7.28 | e . |
| 02 (\$) | : | 9.31 | 9.20 | 9,14 | 9.09 | 9.05 | 9.16 | · , 'a |
| CARB FLOW(g/s) | : | 13.017 | 13.790 | 13.637 | 13.725 | 13.849 | 13.604 | 2.48 |
| | | | | | | 1 | | |
| REYNOLDS NR. | • | 2.83E+04 | | | | · | | |
| REYNOLDS NR. | : | 2.83E+04 | | D | ATE : | 19.3.91 | | |
| TREATED TEST | | | | | | | | |
| TREATED TEST | ; | 2.83E+04 3826 33 | | T | EST MODE: | 1800 rpm | | |
| TREATED TEST | ; | 3826 | | T S | | 1800 rpm 290 | | |
| TREATED TEST ENG. HOURS AMB. TEMP (C) | ; | 3826 33 | TEST 2 | T S F | EST MODE: TACK(mm): UEL DENS: | 1800 rpm 290 | AVERAGE | \$ ST.DE |
| TREATED TEST ENG. HOURS AMB. TEMP (C) | ;;; | 3826 33 1020 | TE\$T 2 58 | T S F | EST MODE: TACK(mm): UEL DENS: | 1800 rpm 290 TEST 5 | AVERAGE 57 | |
| TREATED TEST ENG. HOURS AMB. TEMP (C) BAROMETRIC(mb) | ; ; ; | 3826 33 1020 TEST 1 | | T S F TEST 3 | EST MODE: TACK(mm): UEL DENS: TEST 4 | 1800 rpm 290 TEST 5 | | 3.79 |
| TREATED TEST ENG. HOURS AMB. TEMP (C) BAROMETRIC(mb) PRES DIFF (Pa) EXHST TEMP (C) HC (ppm) | | 3826 33 1020 TEST 1 54 | 58 | T S F TEST 3 59 | EST MODE: TACK(mm): UEL DENS: TEST 4 56 | 1800 rpm 290 TEST 5 59 | 57 | \$ ST.DE 3.79 2.33 0.00 |
| TREATED TEST ENG. HOURS AMB. TEMP (C) BAROMETRIC(mb) PRES DIFF (Pa) EXHST TEMP (C) HC (ppm) CO (\$) | | 3826 33 1020 TEST 1 54 189 | 58 198 80 0.04 | T S F TEST 3 59 198 80 0.04 | EST MODE: TACK(mm): UEL DENS: TEST 4 56 200 80 0.04 | 1800 rpm 290 TEST 5 59 200 80 0.04 | 57 197 80.0 0.040 | 3.79 2.33 0.00 0.00 |
| TREATED TEST ENG. HOURS AMB. TEMP (C) BAROMETRIC(mb) PRES DIFF (Pa) EXHST TEMP (C) HC (ppm) CO (\$) CO2 (\$) | ::::::::::::::::::::::::::::::::::::::: | 3826 33 1020 TEST 1 54 189 80 | 58 198 80 | T S F TEST 3 59 198 80 0.04 3.61 | EST MODE: TACK(mm): UEL DENS: TEST 4 56 200 80 | 1800 rpm 290 TEST 5 59 200 80 | 57 197 80.0 0.040 3.59 | 3.79 2.33 0.00 0.00 0.75 |
| TREATED TEST ENG. HOURS AMB. TEMP (C) BAROMETRIC(mb) PRES DIFF (Pa) EXHST TEMP (C) HC (ppm) CO (\$) | | 3826 33 1020 TEST 1 54 189 80 0.04 | 58 198 80 0.04 | T S F TEST 3 59 198 80 0.04 | EST MODE: TACK(mm): UEL DENS: TEST 4 56 200 80 0.04 | 1800 rpm 290 TEST 5 59 200 80 0.04 | 57 197 80.0 0.040 | 3.79 2.33 0.00 |
| TREATED TEST ENG. HOURS AMB. TEMP (C) BAROMETRIC(mb) PRES DIFF (Pa) EXHST TEMP (C) HC (ppm) CO (\$) CO2 (\$) | | 3826 33 1020 TEST 1 54 189 80 0.04 3.58 | 58 198 80 0.04 3.56 | T S F TEST 3 59 198 80 0.04 3.61 | EST MODE: TACK(mm): UEL DENS: TEST 4 56 200 80 0.04 3.63 | 1800 rpm 290 TEST 5 59 200 80 0.04 3.59 | 57 197 80.0 0.040 3.59 | 3.79 2.33 0.00 0.00 0.75 |

PERCENTAGE CHANGE IN FUEL CONSUMPTION ((TREATED-BASE)/BASE*100) : -43.9 \$

........

REMARKS:

| FUEL TECHNOLOGY PTY LT | D | L | ΓY | PT | .OGY | TECHNOL | FUEL | |
|------------------------|---|---|----|----|------|---------|------|--|
|------------------------|---|---|----|----|------|---------|------|--|

. · .

CARBON BALANCE RESULTS

| | : | BUCL - PEAK | DOWNS | 1.0 | CATION : | PEAK DOWNS | | |
|--|---|---|--------------------------------|---|--|--|------------------------------------|--|
| EQUIPMENT | ; | EUCLID CH200 | l. | UN | IT NR. : | 25 | | |
| ENG. TYPE | : | CUMMINS | | MŐ | DEL 1 | KTTA38C | | |
| RATING | 1 | 1350 HP | | FŲ | EL 1 | | | |
| BASELINE | | | | DA | TE : | 15.11.90 | | |
| ENG. HOURS | : | 1883 | | ΤĔ | ST MODE: | 1800 rpm | | |
| AMB. TEMP (C) | : | 30 | | ST | AÇK(mm): | 290 | | |
| BAROMETRIC(mb) | ŧ | 990 | | FU | EL DENS: | | | |
| | | TEST I | TEST 2 | TEST 3 | TEST 4 | TEST 5 | AVERAGE | \$ ST.DEV |
| PRES DIFF (Pa) | 1 | 40 | 39 | 35 | 38 | 40 | 38 | 5.40 |
| EXHST TEMP (C) | | 192 | 196 | 198 | 199 | 201 | 197 | 1.73 |
| HC (ppm) | | | 20 | 20 | 20 | 20 | 22.0 | 20.33 |
| | | 0.01 | 0.02 | 0.02 | 0.02 | 0.01 | 0.016 | 34.23 |
| CO2 (\$) | | | 3.65 | 3,57 | 3.53 | 3.50 | 3,57 | 1.68 |
| 02 (\$) | : | 12.94 | 12.87 | 12.87 | 12.91 | 12.89 | 12.90 | 0.23 |
| CARB FLOW(g/s) |): | 6.242 | 6.212 | 5,745 | 5.913 | 5,986 | 6.019 | 3.47 |
| | | | | | | 1 | | |
| REYNOLDS NR. | ; | 2.55E+04 | | | • | · · _ | | |
| REYNOLDS NR, | : | 2.55E+04 | | DA | TE I | 19.3.91 | | |
| TREATED TEST | • • | | > | | | | | |
| TREATED TEST ENG. HOURS | • | 3208 | | ΤE | ST MODE: | 1800 rpm | | |
| TREATED TEST | • | | | TE S1 | | | | |
| TREATED TEST ENG. HOURS AMB. TEMP (C) | • | 3208 33 | TEST 2 | TE S1 | ST MODE: FACK(mm): JEL DENS; | 1800 rpm 290 | AVERAGE | \$ ST.DEV |
| TREATED TEST ENG. HOURS AMB. TEMP (C) | :: | 3208 33 1020 | TEST 2 32 | TE St Fl | ST MODE: FACK(mm): JEL DENS; | 1800 rpm 290 | AVERAGE 32 | \$ ST.DEV 5.61 |
| TREATED TEST ENG. HOURS AMB. TEMP (C) BAROMETRIC(mb) | ::::::::::::::::::::::::::::::::::::::: | 3208 33 1020 TE\$T 1 35 203 | | TE Si Fl | ST MODE: FACK(mm): JEL DENS: TEST 4 | 1800 rpm 290 TEST 5 | | • 400 X 41 Mel 54 X 44 4 50 50 50 50 |
| TREATED TEST ENG. HOURS AMB. TEMP (C) BAROMETRIC(mb) PRES DIFF (Pa) | : ::):):): | 3208 33 1020 TE\$T 1 35 203 | 32 205 | TE ST FU TEST 3 30 206 20 | ST MODE: FACK (mm): JEL DENS: TEST 4 33 206 10 | 1800 rpm 290 TEST 5 32 207 | 32 | 5.61 |
| TREATED TEST ENG. HOURS AMB. TEMP (C) BAROMETRIC(mb) PRES DIFF (Pa) EXHST TEMP (C) HC (ppm) | : ::):):): | 3208 33 1020 TEST 1 35 203 10 | 32 205 0 | TE ST FU TEST 3 30 206 20 | ST MODE: FACK (mm): JEL DENS: TEST 4 33 206 10 | 1800 rpm 290 TEST 5 32 207 | 32 205 | 5.61 |
| TREATED TEST ENG. HOURS AMB. TEMP (C) BAROMETRIC(mb) PRES DIFF (Pa) EXHST TEMP (C) HC (ppm) CO (\$) | ::)::)::;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;; | 3208 33 1020 TEST 1 35 203 10 0.02 | 32 205 0 | TE ST FU TEST 3 30 206 20 | ST MODE: FACK (mm): JEL DENS: TEST 4 33 206 10 | 1800 rpm 290 TEST 5 32 207 20 | 32 205 12.0 | 5.61 0.74 69.72 |
| TREATED TEST ENG. HOURS AMB. TEMP (C) BAROMETRIC(mb) PRES DIFF (Pa) EXHST TEMP (C) HC (ppm) CO (\$) | ::::::::::::::::::::::::::::::::::::::: | 3208 33 1020 TEST 1 35 203 10 0.02 3.30 | 32 205 0 0.01 | TEST 3 30 206 20 0.02 | ST MODE: FACK (mm): JEL DENS: TEST 4 33 206 10 0.0! | 1800 rpm 290 TEST 5 32 207 20 0.02 | 32 205 12.0 0.016 | 5.61 0.74 69.72 34.23 |
| TREATED TEST ENG. HOURS AMB. TEMP (C) BAROMETRIC(mb) PRES DIFF (Pa) EXHST TEMP (C) HC (ppm) CO (\$) CO2 (\$) | ::::::::::::::::::::::::::::::::::::::: | 3208 33 1020 TEST 1 35 203 10 0.02 3.30 | 32 205 0 0.01 3.21 | TE ST FU TEST 3 30 206 20 0.02 3.31 | ST MODE: FACK (mm): JEL DENS: TEST 4 33 206 10 0.0! 3.27 | 1800 rpm 290 TEST 5 32 207 20 0.02 3.28 | 32 205 12.0 0.016 3.27 | 5.61 0.74 69.72 34.23 1.19 |

PERCENTAGE CHANGE IN FUEL CONSUMPTION ((TREATED-BASE)/BASE*100) : -15.4 \$

REMARKS:

FUEL TECHNOLOGY PTY LTD

CARBON BALANCE RESULTS

.

a da

| COMPANY · I | | | | | PEAK DOWNS | | |
|--|---|--|--|---|--|---|---|
| EQUIPMENT : | EUCLID CH20 | 0 | UN | IT NR. : 6 | 54 | | |
| ENG. TYPE : | CUMMINS | | MO | DEL : K | TTA38C | | |
| RATING : | 1350 HP | | FU | IEL : | | | |
| BASELINE | | | DA | TE : (| 15.11.90 | | |
| ENG. HOURS : | 689 | | TE | ST MODE: | 1800 rpm | | |
| AMB. TEMP (C) ; | 32 | | ST | ACK(mm): | 290 | | |
| BAROMETR(C(mb): | 988 | | ۴U | JEL DENS: | | | |
| | TEST ! | TEST 2 | TEST 3 | TEST 4 | TEST 5 | AVERAGE | \$ ST.DEV |
| PRES DIFF (Pa): | 59 | 60 | 58 | 58 | 58 | 59 | 1.53 |
| EXHST TEMP (C): | 180 | 183 | 186 | 189 | 190 | 186 | 2.24 |
| HC (ppm) 1 | | 20 | 20 | 10 | 20 | 16.0 | 34,23 |
| CO (≸) : | | 0.01 | 0.01 | 0.01 | 0.01 | 0.010 | 0.00 |
| CO2 (%) : | | | 3.70 | 3.74 | | 3.75 | 1.23 |
| | 14.45 | 14.33 | 14.26 | 14.25 | 14.24 | 14.31 | . 0.61 |
| 02 (%) 1 | 14.42 | | | | | | |
| | | 8,009 | 7.725 | 7.770 | 7.732 | 7.863 | 2,14 |
| CARB FLOW(g/s): | 8.081 | | 7.725 | 7.770 | 7,732 | 7,863 | 2,14 |
| CARB FLOW(g/s): REYNOLDS NR. : TREATED TEST | 8.081 | | | | 7.732 I | 7,863 | 2,14 |
| CARB FLOW(g/s): REYNOLDS NR. : TREATED TEST | 8,081 3.18E+04 | | D/ | | ۱ <u>.</u> | 7.863 | 2,14 |
| CARB FLOW(g/s): REYNOLDS NR. : TREATED TEST ENG. HOURS : | 8,081 3.18E+04 | | D/ TE | ATE : | 1 | 7,863 | 2,14 |
| CARB FLOW(g/s): REYNOLDS NR. ; TREATED TEST ENG. HOURS : AMB. TEMP (C) : | 8,081 3.18E+04 2027 | | D/ TE S ⁻ | ATE : EST MODE: | 1. 19.3.91 1800 rpm | 7,863 | 2,14 |
| CARB FLOW(g/s): REYNOLDS NR. ; TREATED TEST ENG. HOURS : AMB. TEMP (C) : | 8,081 3,18E+04 2027 33 | | D/ TE S ⁻ | ATE ; EST MODE; TACK(mm); UEL DENS; | 1. 19.3.91 1800 rpm | AVERAGE | |
| CARB FLOW(g/s): REYNOLDS NR. : TREATED TEST ENG. HOURS : AMB. TEMP (C) : BAROMETRIC(mb): PRES DIFF (Pa): | 8,081 3,18E+04 2027 33 1020 | 8,009 | D/ TE S' F(| ATE ; EST MODE; TACK(mm); UEL DENS; | 19.3.91 1800 rpm 290 | | ≸ ST.DE |
| CARB FLOW(g/s): REYNOLDS NR. : TREATED TEST ENG. HOURS : AMB. TEMP (C) : BAROMETRIC(mb); | 8,081 3.18E+04 2027 33 1020 TEST 1 | 8,009 TEST 2 | DA TE S' F(TEST 3 | ATE : EST MODE: TACK(mm): UEL DENS: TEST 4 | 19.3.91 1800 rpm 290 TEST 5 | AVERAGE | 2,14 % ST.DE 2.96 1.04 |
| CARB FLOW(g/s): REYNOLDS NR. : TREATED TEST ENG. HOURS : AMB. TEMP (C) : BAROMETRIC(mb): PRES DIFF (Pa): EXHST TEMP (C): HC (ppm) : | 8.081 3.18E+04 2027 33 1020 TEST 1 57 185 10 | 8,009 TEST 2 57 187 10 | D/ TE S ⁻ F(TEST 3 55 187 20 | ATE : EST MODE: TACK(mm): UEL DENS; TEST 4 55 189 10 | 19.3.91 1800 rpm 290 TEST 5 59 190 10 | AVERAGE 57 188 12.0 | \$ ST.DE 2.96 1.04 |
| CARB FLOW(g/s): REYNOLDS NR. ; TREATED TEST ENG. HOURS : AMB. TEMP (C) : BAROMETRIC(mb); PRES DIFF (Pa): EXHST TEMP (C): HC (ppm) : CO (\$) : | 8.081 3.18E+04 2027 33 1020 TEST 1 57 185 10 0.01 | 8,009 TEST 2 57 187 10 0.01 | D/ TE S' F(TEST 3 55 187 20 0.01 | ATE : EST MODE: TACK(mm): JEL DENS; TEST 4 55 189 10 0.01 | 19.3.91 1800 rpm 290 TEST 5 59 190 10 0.01 | AVERAGE 57 188 12.0 0.010 | \$ ST.DE 2.96 1.04 37.27 0.00 |
| CARB FLOW(g/s): REYNOLDS NR. : TREATED TEST ENG. HOURS : AMB. TEMP (C) : BAROMETRIC(mb): PRES DIFF (Pa): EXHST TEMP (C): HC (ppm) : CO (\$) : CO (\$) : | 8,081 3,18E+04 2027 33 1020 TEST 1 57 185 10 0,01 3,38 | 8,009 TEST 2 57 187 10 0.01 3,37 | D/ TE S' F(TEST 3 55 187 20 0.01 3.36 | ATE : EST MODE: TACK(mm): UEL DENS: TEST 4 55 189 10 0.01 3.29 | 19.3.91 1800 rpm 290 TEST 5 59 190 10 0.01 3.40 | AVERAGE 57 188 12.0 0.010 3.36 | \$ ST.DE 2.96 1.04 37.27 0.00 1.25 |
| CARB FLOW(g/s): REYNOLDS NR. : TREATED TEST ENG. HOURS : AMB. TEMP (C) : BAROMETRIC(mb): PRES DIFF (Pa): EXHST TEMP (C): HC (ppm) : CO (\$) : CO (\$) : | 8,081 3,18E+04 2027 33 1020 TEST 1 57 185 10 0,01 3,38 | 8,009 TEST 2 57 187 10 0.01 | D/ TE S' F(TEST 3 55 187 20 0.01 | ATE : EST MODE: TACK(mm): JEL DENS; TEST 4 55 189 10 0.01 | 19.3.91 1800 rpm 290 TEST 5 59 190 10 0.01 | AVERAGE 57 188 12.0 0.010 | \$ ST.DE 2.96 1.04 37.27 0.00 1.25 |
| CARB FLOW(g/s): REYNOLDS NR. : TREATED TEST ENG. HOURS : AMB. TEMP (C) : BAROMETRIC(mb): PRES DIFF (Pa): EXHST TEMP (C): HC (ppm) : CO (\$) : CO2 (\$) : | 8,081 3,18E+04 2027 33 1020 TEST 1 57 185 10 0,01 3,38 12,54 | 8,009 TEST 2 57 187 10 0.01 3,37 | D/ TE S ⁻ F(TEST 3 55 187 20 0.01 3.36 12,48 | ATE : EST MODE: TACK(mm): UEL DENS: TEST 4 55 189 10 0.01 3.29 | 19.3.91 1800 rpm 290 TEST 5 59 190 10 0.01 3.40 12.42 | AVERAGE 57 188 12.0 0.010 3.36 | \$ ST.DE 2.96 1.04 |

PERCENTAGE CHANGE IN FUEL CONSUMPTION ((TREATED-BASE)/BASE*100) : -10.6 \$

1

REMARKS:

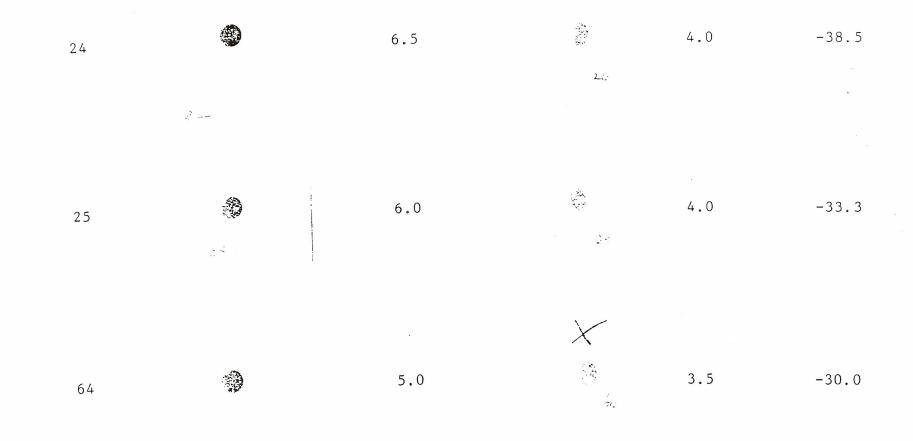
APPENDIX III ASTM D2156-63T, BACHARACH SMOKE PATCHES

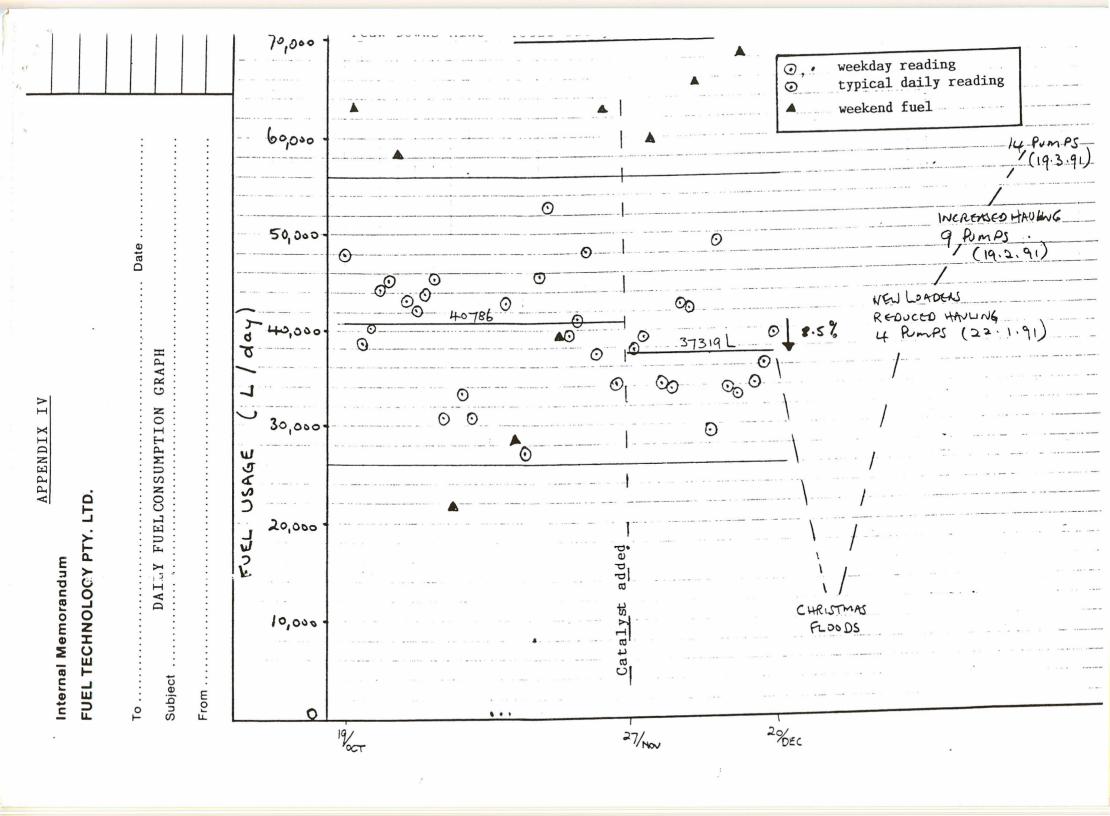
.

(BHP-UTAH COAL LTD - PEAK DOWNS MINE)

.

HAULER NO UNTREATED (15.11.90) BACHARACH NO TREATED (19.3.91) BACHARACH NO % CHANGE





PEAK DOWNS MINE - CATALYST FUEL CONSUMPTION TRIAL

A. ANALYSIS OF MINE DATA AS PRESENTED BY AA LITTLE.

i. The fuel improvements of 16-37% as derived from the data are higher than can be attributable to catalyst addition alone.

2. The following observations are made:

(i) The service bay fuel meter recorded explosives fuel up until 19th October, 1990. Explosives fuel use from 3.10.90-17.7.91 (39 weeks) totalled 664058 L, being an average 17,027 L/week. This figure should be used to correct the service bay fuel figures.

(ii) Unit TKH464 recorded an exceptionally large jump in consecutive meter readings from 51162 to 54525 hours (ie 3363 hrs) from 8.11.90-29.11.90. Average weekly usage rate at about that time was 81 hrs for this unit. This adjustment should be used to correct data. This error is the major reason for the extreme variation noted during Nov. '90.

(iii) The week ending 14.11.90 was marked by FEDFA disputes on 3 days. The L/hr figures for this week appear at an exceptionally low level. No cause could be found to explain this, and it is recommended that this week's data be deleted from the comparison.

(iv) The entries for estimated pump hours into the computer programme are out of sequence by i week, with the actual data collected.

B. METHODS OF COMPARISON.

1. To achieve better accuracy in this comparison, it is necessary to isolate data for the original fleet used prior to catalyst treatment. Two elements contained in the post-treatment data must be eliminated to enable this to be achieved.

2 7 1

(i) removal of fuel component due to pump usage.

(ii) removal of fuel component due to the 2 new Le Torneau Lii00 loaders.Calculations were made as follows;

(i) Dewatering pumps. Following data used:

Estimated pump hours/wk..... as per data provided Aver pump HP = 230 Duty level of engine = 75% (not pump) Specific Fuel Consumption = .224L/HPhr (This is typical industry standard)

Pump Fuel = .224 x 230 x 75% x weekly pump hours

= 38.64 L/hr

(ii) The distributors of the Le Torneau L1100 loaders advise that fuel consumption is expected at 120-130 L/hr. For estimations, 120L/hr usage rate was used to adjust data.

2. The recommended corrections and above estimations are necessary to enable realistic comparison of the data. They also permit comparison of the performance of the catalyst on the "original fleet", as well as greatly reducing the variation and magnitude of the measured benefit.

| | DATE | Service Bay | Service Bay | Pump Fuel | Service Bay | New Loaders | Service Bay | Major | Corrected | Corr. | Corr. | P 1 | | | |
|-----------------------|--------------------------------|---|---|--|--|--|--|-------------------------------------|-------------------------------------|--------------------------------------|-------------------------------------|---|--|--|--|
| | | Records | corrected for Explos | Estim. | less Pump est. | Fuel Estim. | less Pump & Loaders est | Plant | Maj. Plant Error in | Plant plus | Plant less | | consum Litres/ | - | |
| | | L _i | L ₂ | | L3 | | L ₄ | H | TKH464 H ₂ | Pumps H ₃ | Loaders ^H 4 | L ₂ /H ₂ | L ₂ /H ₃ | L3/H2 | L ₄ /H ₄ |
| 0 C T 9 0 | 10 17 24 31 Av | 266586 244731 247263 233220 | 249559 227704 242398 233220 | 9042 9042 9042 9042 9042 | 240517 218662 233356 224178 | - - - - | 240517 218662 233356 224178 | 2725 2676 2621 2791 | 2725 2676 2621 2791 | 2959 2910 2855 3025 | 2725 2676 262i 279i | 91.6 85.1 92.5 83.6 88.1 | 84.3 78.2 84.9 77.i 81.i | 88.3 81.7 89.0 80.3 84.8 | 88.3 8i.7 89.0 80.3 84.8 |
| N O V | 7 i4 2i 28 Av | 207424 106711 224255 200078 | 207424 i067ii 224255 200078 | i4992 i4992 i4992 i4992 i4992 | i92432 9i7i9 209263 i85086 | | 192432 91719 209263 185086 | 253i 2960 3540 3729 | 253i i920 2500 2689 | 2919 2308 2888 3077 | 253i 1920 2500 2689 | 82.0 55.6 89.7 74.4 81.8 | 71.1 46.2 77.7 65.0 71.1 | 76.0 47.8 83.7 68.8 76.0 | 76.0 47.8 83.7 68.8 87.9 |
| D E C | 5 12 19 26 Av | 204815 228882 205437 140727 | 204815 228882 205437 140727 | 14992 14992 14992 24807 | 189823 213890 190445 115920 | - 4080 2400 | 189823 213890 186365 113520 | 2519 2707 2514 1512 | 2519 2707 2514 1512 | 2907 3095 2902 2154 | 2519 2707 2480 1492 | 8i.3 84.6 8i.7. 93.i 84.3 | 70.5. 74.0 70.8 65.3 70.5 | 75.4 79.0 75.8 76.7. 76.7 | 75.4 79.0 75.i 76.i 76.5 |
| J A N 9 i | 2 9 16 23 30 Av | i05029 83429 i82008 223533 226502 | i05029 83429 i82008 223533 226502 | 24807 24807 34390 34390 34390 39181 | 80222 58622 147618 189143 187321 | 2400 i0320 i1400 i6560 i0200 | 77822 48302 136218 172583 177121 | 8i4 115i 1920 2643 2473 | 8i4 1151 1920 2643 2473 | 1456 1793 2810 3553 3487 | 794 1065 1825 2505 2388 | i29.0 72.5 94.8 84.6 91.6 91.2 | 72.1 46.5 64.8 62.9 65.0 62.6 | 98.6 50.9 76.9 71.6 75.7 73.7 | 98.0 45.4 74.6 68.9 74.2 71.4 |
| F E B | 6 13 20 27 Av | 189850 236845 228440 313435 | 189850 236845 228440 313435 | 39181 39181 35549 35549 | 150669 197664 192891 277886 | i4640 i7760 i6080 i8i20 | 136029 179904 176811 259766 | 1964 2949 2634 3352 | 1964 2949 2634 3352 | 2978 3963 3554 4272 | 1842 2801 2500 3201 | 96.7 80.3 86.7 93.5 88.9 | 63.8 59.8 64.3 73.4 65.6 | 76.7 67.0 73.2 82.9 75.2 | 73.8 64.2 70.7 81.2 72.7 |
| M A R | 6 13 20 27 Av | 294837 292458 257740 249569 | 294837 292458 257740 249569 | 35549 35549 35549 35549 | 259288 256909 222191 214020 | 22200 24000 22320 20520 | 237088 232909 199871 193500 | 2947 3442 3070 2792 | 2947 3442 3070 2792 | 3867 4362 3990 3712 | 2762 3242 2884 2621 | i00.0 85.0 84.0 89.4 89.3 | 76.2 67.0 64.6 67.2 68.7 | 88.0 74.6 72.4 76.7 77.7 | 85.8 71.8 69.3 73.8 75.0 |
| A P | 3 | 180556 | 180556 | 35549 | 145007 | 12600 | i32407 | 1997 | 1997 | 2917 | 1892 | 90.4 | 61.9 | 72.6 | 70.0 |

* Deleted - data well outside normal range (3 days FEDFA strike)

